

Research article

Supercritical extraction and microwave activation of wood wastes for enhanced syngas production and generation of fullerene-like soot particles

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ARTICLE INFO

Keywords:

Biomass
Pyrolysis
Gasification
Carbon dioxide
Biorefinery
Nanomaterials

ABSTRACT

This work demonstrated that supercritical carbon dioxide extraction is effective as a pre-treatment technology to generate soot particles with the fullerene-like structure and increase syngas yield from extracted residues during coupled microwave activation with gasification. Supercritical carbon dioxide extraction removes over half of the fatty and resin acids from needles and branches, whereas the extraction of needles generates greater yields of value-added compounds. The high yields of extractives indicate the effective conversion of waste wood for the sustainable production of value-added chemicals. The wood extraction did not influence the solid residue yields during pyrolysis/gasification emphasizing the significant potential of integrating the extraction process into the holistic biorefinery. Interestingly, supercritical carbon dioxide extraction had a significant effect on the structure and quality of soot particles formed. The differences in the extractives composition led to the formation of needle soot particles with a porous and less ordered nanostructure, whereas the soot branches obtained a ring graphitic structure. The greater yields of steroids and terpenes during the extraction of needles compared to the branches pretreatment indicated the influence of the extractives type on the soot nanostructure.

1. Introduction

Biomass is a renewable and widely available resource that can be used for heat, power, as a feedstock for liquid fuels and as a sustainable chemical production [1]. The cost-efficient development of biorefineries depends on feedstock flexibility and effective pre-treatment processes for chemical production in combination with efficient power and heat generation [2]. The pre-treatment processes decrease the water content in feedstock, increase energy density, and generate high value-added products for the chemical industry. Remaining solid fuel fractions are used for the generation of renewable and clean energy. Little is known about the effect of supercritical CO₂ (scCO₂) extraction on the yields and properties of products from high-temperature pyrolysis and gasification.

In the forestry sector, utilizing the supercritical extraction process has been shown to improve the off-gassing of wood pellets, thus

reducing the potential for uncontrolled auto-oxidation, while maintaining pellet properties [3,4]. Moreover, supercritical CO₂ extraction can also improve the physicochemical properties of solid char from pyrolysis at high temperatures, leading to greater electric conductivity and low reactivity of solid char [5]. Supercritical CO₂ extraction increases the bending strength and stiffness of residual wood and thus, decreases the cost of process scaling up, wood storage and transportation [6]. Several methods exist for the extraction of high-value molecules from biomass including conventional organic solvent extraction, hydrodistillation, low-pressure solvent extraction and hydrothermal feedstock processing [7–9]. Supercritical fluids demonstrate properties between those of a liquid and a gas, with the viscosity of a supercritical fluid being an order of magnitude lower than a liquid, whereas the diffusivity is an order of magnitude higher and thus, leading to the enhanced heat and mass transfer [10]. The properties of a solvent can be fine-tuned by varying the temperature and pressure. Conventional

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<https://doi.org/10.1016/j.fuproc.2020.106633>

Received 12 May 2020; Received in revised form 22 August 2020; Accepted 2 October 2020

Available online 15 October 2020

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solvents traditionally utilized in wax extraction (such as hexane) are frequently viewed as being problematic due to the toxicological and environmental impacts [11]. Supercritical fluid extraction using CO₂ as a solvent has an easily accessible critical point, is non-flammable, has minimal toxicity and is widely available [12]. Supercritical CO₂ extraction has been conducted on a commercial scale for over two decades for the extraction of products from biomass [13]. Thus, the proposed biorefinery concepts [14–16], which combine the scCO₂ extraction and pyrolysis processes, will be considered in the present work for the use of low value-added forestry residues for the cost-efficient production of extracted value-added products and remaining solid feedstock for further use in the production of bio-oil using microwave pyrolysis and syngas using fast pyrolysis [17,18].

The advantage of pyrolysis is that the yield of end-products can be altered depending on the operating conditions, whereas the heat treatment temperature and the heating rate are known to have most influence on the product yield and composition [19,20]. The combination of scCO₂ extraction process with microwave pyrolysis has been rarely studied in the literature. However, microwave pyrolysis has been previously shown to be an energy efficient process for biomass conversion and has become widely accepted as a mild and controllable processing tool [21]. Microwave pyrolysis has been carried out at temperatures below 350°C due to the high pyrolysis rates, good energy efficiency and better controllability than conventional pyrolysis [22,23]. Microwave pyrolysis converts biomass into high-quality bio-oil for chemicals and solid char that is a valuable feedstock for heat and power generation [24]. The combination of a low temperature microwave pyrolysis with scCO₂ extraction could provide better control over the biomass decomposition and a better separation of undesirable water and water-soluble components in the bio-oil and thus get closer to fuel-ready oils than what has previously been achieved. Moreover, the combination of supercritical carbon dioxide extraction with microwave pyrolysis will improve the total process efficiency due to the low solid product yields and the better quality of bio-oil [24].

Forest industry produces millions of tons of waste wood residues which are ideally suited for exploitation by a combination of green technologies for the generation of value added products. Wood chemical composition varies with tree part (root, stem, or branch), type of wood, geographic location, climate and soil conditions [25]. The mineral content and distribution of lignocellulosic compounds show significant variations between tree parts (needles, branches, stem, bark, etc.) [26]. Spruce needles have high phosphorus, sulfur, potassium and calcium contents, whereas the spruce bark contains high amounts of calcium and magnesium [27,28]. The ash and extractives contents are higher in pinewood bark compared to stemwood [29], whereas branches and root samples contain more minerals, galactan, xylan and lignin compared to glucomannan rich stemwood [30]. Compared to wood, needles are richer in extractives, especially waxes [31,32]. A recent study has demonstrated that supercritical carbon dioxide extraction had little impact on the physical properties of original wood nor on the yield of solid char using conventional pyrolysis. Importantly, a mixture of different low quality wood fractions was able to yield chars with reactivity and dielectric properties approaching that of fossil-based metallurgical coke [33]. However, the effect of supercritical carbon dioxide extraction on the properties of liquid products and gas in the conventional pyrolysis and products from fast pyrolysis at temperatures greater than 900°C has been rarely studied. Microwave heating of biomass and organic wastes creates challenges due to the poor microwave adsorbance of various carbon materials leading to an incomplete conversion, and thus, high yields of solid char in pyrolysis [34,35]. The remaining char from the microwave pyrolysis has a potential to be used as a feedstock in the combustion and gasification processes [36]. In the present study, the properties of solid char from microwave pyrolysis using remaining solid feedstock after scCO₂ extraction were further tested in the entrained flow gasification reactor [37,38].

Forest industry produces millions of tons of waste wood residues

which can be used in a closed loop efficient process. Supercritical extraction followed by biomass microwave pyrolysis has a high potential to remove extractives and other volatile compounds, and thus, to produce a high quality bio-oil and value-added feedstock for gasification and combustion. Understanding the properties of wood fractions (bark, stem, needles, branches) is important for: (1) optimizing solvent extraction processes leading to maximal yields of extractives and (2) optimizing the char yield in high-temperature processes. To the author's knowledge, no previous work has been carried out on the characterization of solid char from microwave pyrolysis for the use in fast pyrolysis as a pre-step for gasification and combustion. The main objective of this work is to demonstrate that the removal of extractives from low value forest residues using scCO₂ treatment provides both an added-value product for the chemical industry as well as yielding a valuable feedstock for the production of char in microwave pyrolysis and fast pyrolysis for the energy sector.

2. Materials and methods

On average, 147 year old Scots pine trees in northern Sweden were harvested from a forest stand. Fractions from harvested trees were green needles, and branches without needles. Prior to the scCO₂ extraction and microwave pyrolysis, wood fractions were comminuted on a hammer mill (MAFA EU-4B manufacturer) with an operating speed of 60 Hz. ScCO₂ extraction was performed on different pinewood fractions. Solid residues were collected after extraction and dried at room temperature. The extractives were collected and weighed for the calculation of yields. The composition of volatiles in non-treated wood fractions and samples after scCO₂ extraction was investigated by pyrolysis-gas chromatography/mass spectrometry (Py-GC/MS). The branches after CO₂ extraction were pyrolyzed in the microwave furnace, whereby the char and bio-oil yields were measured. The collected char was further reacted at 1100°C in the drop tube furnace (DTF) under pyrolysis and CO₂ gasification conditions. Soot nanostructure and particle size were studied using microscopy. The effects of scCO₂ extraction and fast pyrolysis conditions on the wood char and soot reactivity were investigated using a thermogravimetric analyzer.

2.1. Supercritical CO₂ extraction

The scCO₂ extractions were conducted using a supercritical extractor SFE 500 (Thar technologies, USA). Supercritical fluid grade carbon dioxide (99.99%, dip-tube liquefied CO₂ cylinder obtained from BOC) was used in the extractions. The CO₂ supplied from a cylinder as a liquid was maintained in this state through a cooling unit (−2°C) to avoid cavitation in the high pressure pump. ScCO₂ extractions of the different biomass types were optimized using a two-level factorial design [3]. Evaluation was made by determination of the extracts' weight in the different experiments. Approximately 180 g of biomass was placed into the 500 mL extraction vessel. The reaction vessel was heated to the required temperature and was equilibrated for 5 min. An internal pump was used in order to obtain the required pressure. The system was run in a dynamic mode, in which the carbon dioxide containing the extractives flowed into the collection vessel. A flow rate of 40 g min^{−1} of liquid CO₂ was applied and the extraction was carried out for 2 h. On completion the system was depressurized over a period of 60 min. The conditions chosen (400 bar and 60°C) for the scCO₂ extraction of the needles and branches were based on optimisation studies in the literature [39]. Pressure and temperature are known to be related to density of CO₂ that needs to be incorporated in order to maximise the % crude extract [40]. The conditions chosen (400 bar and 60°C) for the scCO₂ extraction are the optimal conditions leading to the highest extraction rates [33].

2.2. Microwave pyrolysis

Fifty gram of scCO₂ extracted branches were weighed and exposed to a maximum microwave power of 1200 W using a rotative solid phase microwave reactor ROTO SYNTH (Milestone, Italy) fitted with a vacuum module VAC 2000 in series. The sample was heated at a rate of 17 °C min⁻¹ to a maximum temperature of 180°C. Based on previous work [5,41], the heating rate and the heat treatment temperature were selected to obtain the maximal yield of liquid fractions and to minimize the char yield. Liquid fractions were collected via the vacuum unit that collected and condensed vapours during pyrolysis. The char yield was determined by weighing the sample before and after microwave treatment, as discussed by Budarin et al. [24].

The liquid products collected by the condensers from the microwave pyrolysis were rinsed with dichloromethane (DCM), as described in the previous work [37,42]. The oil fraction in the liquid mixture was separated out and concentrated to a detection level using a Genevac Rocket Evaporation system. The oil fraction composition was then determined using a Varian CP-3800 GC coupled with a Varian Saturn 2200 mass spectrometer (MS). The conditions for the GC/MS equipment were: GC injector port temperature 290°C; transfer line temperature 280°C; manifold temperature 120°C and trap temperature 200°C; the oven program temperature was 40°C for 2 min, then it was ramped to 280°C with 5°C min⁻¹, and finally held at 280°C for 10 min. The compounds in the oil were quantified using external standards.

2.3. Fast pyrolysis in drop tube reactor

The feedstock was reacted at 1100°C in a laminar drop tube reactor. The DTR setup was described in detail by Trubetskaya et al. [43] and shown in Fig. 1. Based on previous work [44], operation at 1100°C was selected to simulate the operating conditions in an industrial-scale entrained-flow gasifier. The reactor consists of an alumina tube (internal diameter: 54 mm, heated length: 1.06 m) heated by four heating elements with independent temperature control. Gas flow rate into the reactor is regulated by mass flow controllers (EL-FLOW® Select, Bronkhorst High-Tech B.V.). The feeding system is based on a syringe pump that displaces a bed of fuel that falls directly into the high temperature zone in the reactor through a water-cooled probe. The syringe pump was vibrated to ensure stable feeding of the fuel particles. In each experiment, ≈ 5 g of biomass or char was fed into the reactor at a rate of 0.2 g min⁻¹. Both primary (0.18 L min⁻¹ measured at 20°C and 101.3 kPa) and secondary (4.8 L min⁻¹ measured at 20°C and 101.3 kPa) feed gases were N₂. The residence time of fuel particles was estimated to be about 1 s, taking into account density changes during pyrolysis. Reaction products were separated into coarse particles (mainly char and fly ashes), fine particles (mainly soot and ash aerosols), permanent gases, and tars. Coarse particles were captured in a cyclone (cut size 2.5µm). Soot particles exited the cyclone and were collected on a grade QM-A quartz filter with a diameter of 50 mm (Whatman, GE Healthcare Life Science).

The carbon and hydrogen balances using the experimental data of yields and composition of gas and solid products represent an average of two measurements, as described in the previous work [20,45]. Solid products were categorized as char, soot, and coke. Char and soot were collected in a char bin and on a filter, respectively. Char is the fraction of non-devolatilized solid present in the initial biomass, consisting mainly of carbon and ash. Coke, the carbonaceous material deposited on the reactor walls, was quantified after each experiment by measurement of the concentration of CO₂ during oxidation. Water, vapor, tars, and large hydrocarbon yields (organics+vapor) were not measured directly, instead estimated by gravimetric differences.

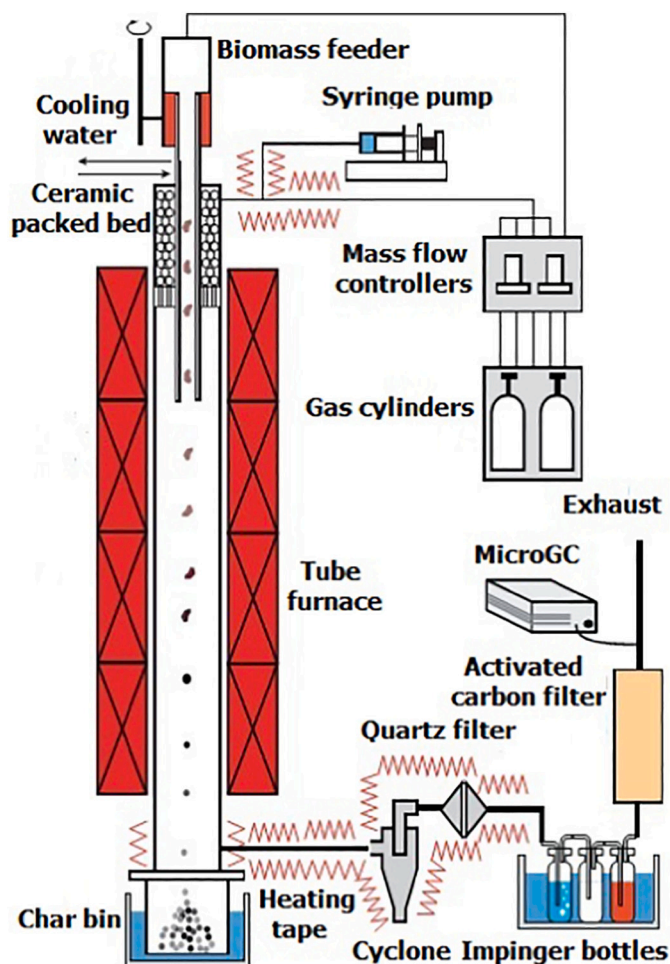


Fig. 1. Schematic view of the drop tube reactor implemented in this study.

2.4. Product characterization

2.4.1. Elemental analysis

The elemental analysis was performed on an Analyzer Series II (Perkin Elmer, USA), according to the procedure described in ASTM D5373-02. Acetanilide was used as a reference standard. The oxygen content was calculated by difference.

2.4.2. Proximate analysis

The proximate analysis was conducted to determine the contents of moisture, ash, volatiles, and fixed carbon according to the procedures described in ASTM D2216-19, ASTM D1102-84, ASTM D3175-11, and ASTM D3172-13. The high heating value was determined by the bomb calorimeter (IKA C-200) according to the procedure described in ASTM D2015-85.

2.4.3. Ash compositional analysis

The ash compositional analysis was performed by ICP-OES in ASTM D6349-13. Prior to the analysis, biomass samples were pre-heated in oxygen at 10°C min⁻¹ up to 550°C and kept at that temperature for 7 h.

2.4.4. Thermogravimetric analysis

The char samples from the microwave treatment and the char and soot samples from the further high-temperature pyrolysis and CO₂ gasification in the drop tube reactor were firstly crushed to a fine powder in a mortar with a ceramic pestle. The thermal decomposition of samples was determined using a thermogravimetric instrument STARE System (Mettler Toledo, USA) by loading 5 mg of sample in Al₂O₃

crucible.

The initial sample mass and heating rates used in the TG experiments were selected to minimize possible mass transfer limitations that may occur by O₂/CO₂ gasification concentration gradients through the TG crucible down to the particle bed, through the particle bed, and inside the soot and char particles [46,47]. The previous results [48] showed that less than 5 mg of char and soot samples should be applied to avoid mass transfer limitations using a heating rate of 10°C min⁻¹ in 40% volume fraction CO₂ gasification. The kinetic parameters of char and soot samples were derived by the integral method presented by Coats and Redfern [49]. Through integral transformation and mathematical approximation, the linear equation was expressed in the form:

$$\ln\left(-\frac{\ln(1-X)}{T^2}\right) = \ln\left(\frac{A \cdot R}{\kappa \cdot E_a}\right) - \frac{E_a}{R \cdot T} \quad (1)$$

In Eq. (1), κ is the heating rate and R is the gas constant. A plot of $\ln(-\ln(1-X) T^{-2})$ versus T^{-1} gives a straight line whose slope and intercept determine the values of the activation energy (E_a) and pre-exponential factor (A). The previous results [20,50] showed that a first order reaction model in both solid residue mass and gasification agent can describe the experimental results well.

2.5. Feedstock characterization

2.5.1. Py-GC/MS

The Py-GC/MS analysis was conducted on non-treated needles and branches and samples after scCO₂ extraction using a Trapping Pyrolysis Autosampler 5250-T (CDS Analytical, UK) coupled to a gas chromatography unit 7890 (Agilent Technologies, USA) and a mass spectrometer 5977A (Agilent Technologies, USA). Twenty milligram of wood samples was loaded into a quartz tube and pyrolyzed at 600°C for 10 s. The pyrolysate was separated on a 30 m length, 0.25 mm internal diameter and 0.25 μ m film thickness capillary column DB-5 (Agilent Technologies, USA). The GC was operated at a constant helium flow of 1 mL min⁻¹ and a 50:1 split ratio. The GC inlet and detector temperatures were both 350°C. The oven program started at 40°C for 2 min and was heated up to 300°C at a constant heating rate of 10 K min⁻¹ with a final hold time 30 min. The mass spectrometer ion source was set to 230°C and the interface to 280°C, scanning took place once per second in the range of 50 to 550 *m/z*. Volatile compounds were identified by comparing the mass spectra with NIST Lab database versions 147 and 27 with an identity threshold cut-off of 50. Py-GC/MS experiments were conducted at least in duplicate. More than 130 peaks were displayed on the chromatograms. The major target compounds with a spectral match quality greater than 85% were listed in the supplemental material (Table S-1). The chromatographic signals were integrated and the relative peak areas were calculated. The calculation of total peak area included the identified and unknown compounds in pyrolysis.

2.5.2. TG-FTIR

The temperature resolved composition of volatiles was characterized using a FTIR spectrometer EGA TL 8000 (Perkin-Elmer, USA) coupled to the thermogravimetric analyzer. For the TG-FTIR analysis, ca. 10 mg of a sample and high purge gas flow rates (100 ml min⁻¹) were used in order to optimize the FTIR signal. The wood samples were evenly dispersed on ceramic crucibles, pre-dried at 105°C and heated up to 600°C at a constant heating rate of 10°C min⁻¹. The FTIR instrument equipped with a deuterated triglycine sulfate (DTGS) detector was set to a scan rate of 0.2 cm s⁻¹ and to a resolution of 2 cm⁻¹ in the 4000–450 cm⁻¹ range. Thus, 288 spectra were acquired every 10 s during the heating ramp. The temperatures of the sampling line and the gas cell were kept at 230°C. The pump of the FTIR system constantly extracted 50 mL min⁻¹ from the TGA off-gas through the FTIR gas cell. The spectra interpretation of smaller compounds (H₂O, CH₄, CO₂ and

Table 1

Absorption bands and specific wave numbers used for the gas profiles [51].

Compound	Absorption band, cm ⁻¹	Identification, cm ⁻¹
H ₂ O	4000–3400, 1800–1300	3853
CH ₄	3018	3018
CO ₂	2391–2217	2360
CO	2220–2150, 2140–2060	2186

CO) were identified, assigned and recorded according to the characteristics adsorption data in Table 1. The larger compounds were only grouped and assigned to corresponding bands of adsorption.

2.6. Soot characterization

2.6.1. Soot pretreatment for microscopy

Prior to microscopy, soot samples were kept at 350°C for 4 h in a thermogravimetric instrument to reduce the volatile contents. Samples were dry dispersed on a lacey carbon copper grid.

2.6.2. Transmission electron microscopy

Soot morphology was studied using a FEI Titan transmission electron microscope operated at 120 keV.

2.6.3. Particle size distribution analysis using TEM

The particle size of soot samples was estimated manually from TEM images using the ImageJ software [52,53]. Only clearly visible primary particles were selected for accurate analysis. The data was assessed to establish particle size distributions. For size analysis, soot particles were assumed spherical. Particle size analysis was conducted on 100 particles at each operating condition. Standard deviation was calculated for curvature, fiber length (see definition below) and separation distance of graphene layers as described in the supplemental material (Eq. (1)). The curvature of a single graphene sheet was calculated as shown in the supplemental material (Eq. (2)).

3. Results and discussion

3.1. Biomass characterization

Fuel selection in this study was based on the differences in the ash composition and plant cell compounds (cellulose, hemicellulose, lignin, extractives). The proximate, ultimate and ash compositional analysis of non-treated wood fractions and samples after scCO₂ extraction is shown in Table 2. The compositional analysis of biomass (cellulose, hemicellulose, acid-soluble lignin, acid-insoluble lignin, protein and extractives) was conducted according to NREL technical reports [54–56] and Thammassouk et al. [57], and shown in Table 3.

3.2. Product yields in DTF

The mass balances of needles and branches pyrolysis with respect to measured solid residues (char, soot, coke) and major gaseous products (CO₂, H₂, CO, CH₄, C₂H₄, C₂H₂) are shown in Fig. 2(a). During pyrolysis of needles and branches, mainly gaseous products were formed, along with smaller amounts of solid residues. Almost all hydrogen (> 95%) was found in the form of gaseous products. The differences in product yields of non-treated wood fractions and scCO₂ extracted samples were small. The removal of extractives increases the temperature of hemicellulose and cellulose decomposition only slightly, leading to the reduced influence of supercritical CO₂ extraction on the total char yield during fast pyrolysis at high temperatures [58]. Moreover, the thermogravimetric analysis showed that the char yield from the pyrolysis of extractives was as high as 36% which is similar to the char yields from the pyrolysis of organosolv lignin [59,60].

Table 2
Proximate, ultimate and ash analyses of non-treated Scots pinewood fractions and samples after scCO₂ extraction.

Fuel	Needles		Branches	
	Original	scCO ₂ extracted	Original	scCO ₂ extracted
Proximate and ultimate analysis (% on dry basis)				
Moisture ^a	6.5	5.6	7.3	6.8
Ash (550 °C)	2.2	2.3	0.8	1
Volatiles	80.8	78.8	80.6	70.9
HHV ^b	22.4	21.3	21.7	20.9
LHV ^b	21	20	20.4	19.6
C	53.7	51.8	53.5	51.4
H	6.5	6.3	6.2	5.9
O	36.1	38.2	39.0	41.2
N	1.3	1.4	0.4	0.5
S	0.1	0.1	0.03	0.04
Ash compositional analysis (mg kg ⁻¹ on dry basis)				
Cl	0.02	0.02	< 0.01	0.01
Al	250	200	150	200
Ca	2450	2500	1300	1200
Fe	70	70	60	70
K	5600	5500	2000	1900
Mg	750	800	400	400
Na	25	20	< 10	10
P	1500	1550	400	400
Si	400	380	400	350
Ti	4	3	6	10

^a wt% (as received)

^b in MJ kg⁻¹.

Table 3
Composition of non-treated Scots pinewood fractions and extractives yield after scCO₂ extraction, calculated in percentage based on dry basis (wt%).

Biomass	Cellulose	Hemicellulose	Lignin		Extractives	
			Acid insoluble	Acid soluble	(raw wood)	(after scCO ₂ extraction)
Needles	23.4	15.1	26.5	0.5	12.1	7.9
Branches	25.3	19.4	28	1	8	4.4

The yield of aldehydes and alkanes formed during pyrolysis of extractives was also similar to the yields from original wood pyrolysis, whereas the gas yield was lower during the decomposition of extractives than in wood pyrolysis [60]. Fig. 2(b) illustrated the mass balances of microwave treated char of scCO₂ extracted species in pyrolysis and CO₂ gasification, with the gas yield remaining greater in CO₂ gasification than in pyrolysis due to the homogeneous reaction between CO₂ and volatiles [61]. Fig. 3 illustrates the soot and char yields which are separated into organic matter and ash. The soot yield remained only slightly changed with the supercritical CO₂ extraction, whereas the char yield of branches and needles decreased by approximately 4 and 3% respectively in pyrolysis. Supercritical CO₂ extraction also led to the decrease in the inorganic matter content of needles and char branch samples. The char yield of scCO₂ extracted char branches using microwave pre-treatment was lower in CO₂ gasification than during fast pyrolysis in the drop tube reactor, whereas greater soot yield was obtained in CO₂ gasification, confirming the previous results of Umeki et al. [62]. In general, during high-temperature fast pyrolysis the soot yield of scCO₂ branches from additional treatment using the microwave pyrolysis was lower than the soot yield from scCO₂ extracted branches, as shown in Fig. 3(b).

The pyrolysis and gasification experiments showed that scCO₂ extraction of wood fractions increased syngas yield and had a negligible influence on the solid product yields, as shown in Fig. 2(a) and supplemental material (Fig. S-3(a)). The scCO₂ extraction removed most of

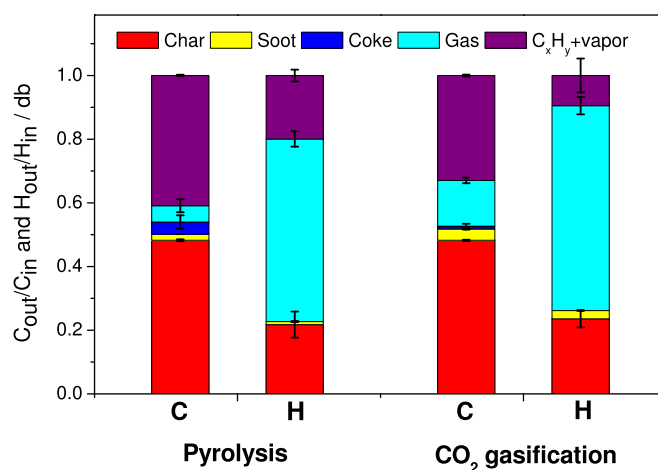
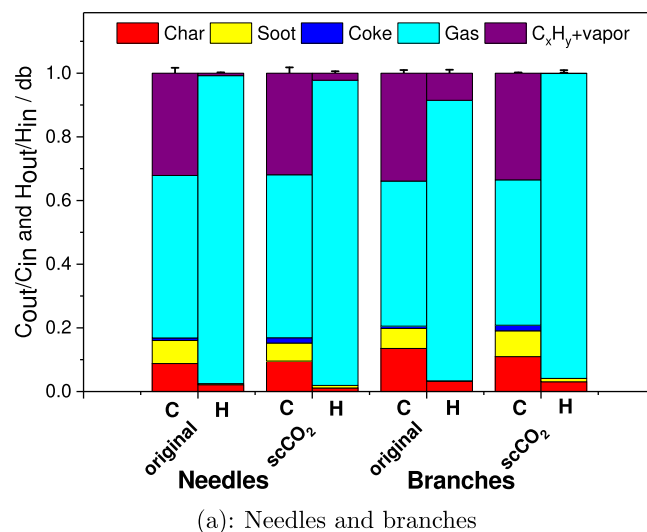
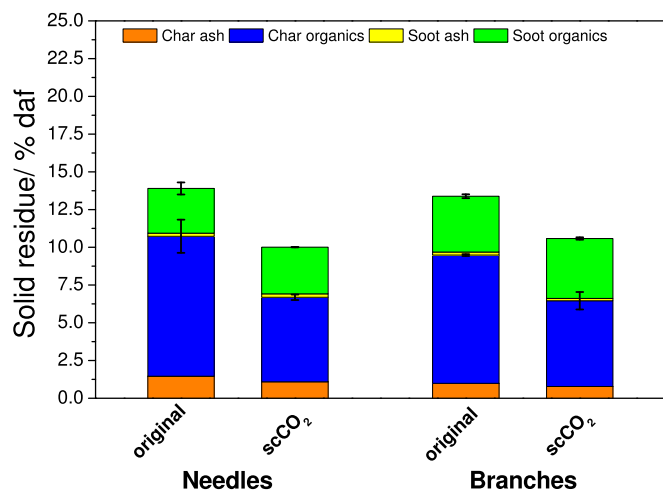


Fig. 2. Carbon and hydrogen distribution of: (a) needles and branches and samples after scCO₂ extraction and (b) from pyrolysis and CO₂ gasification of scCO₂ branches char that was prior treated in the microwave reactor (relative to microwave char).

the resin acids, aromatics and steroids from the wood fraction. Extracted components are more thermally stable and less reactive than the majority of volatile compounds, which lead to the increased yield of syngas during CO₂ gasification. The concentrations of H₂, CO, CO₂ and C_xH_y (CH₄, C₂H₂, C₂H₄) from pyrolysis and gasification are shown in the supplemental material (Fig. S-3(b)). The non-treated branches and scCO₂ extracted sample had a greater concentration of H₂ and CO than needles which contained less cellulose and lignin than branches. Cellulose, with more carbonyl and carboxyl groups, accounted for a greater CO yield, whereas lignin with more methoxylated aromatic ring structures released more H₂ and CH₄ in pyrolysis [63]. Supplemental material (Fig. S-3) shows that scCO₂ extraction led to the greater gas yield with the increased CO₂ and CO formation in needles and branches pyrolysis. The removal of extractives from pinewood enhanced the formation of acetic acid and levoglucosan due to the changes in cellulose fiber orientation [64]. The char yield of microwave char reacted in pyrolysis was slightly greater than the char yield in CO₂ gasification. Compared with pyrolysis of scCO₂ extracted microwave char, the concentration of CO was significantly greater and the concentration of H₂ was slightly lower in CO₂ gasification, as shown in the supplemental material (Fig. S-3). The char yield in CO₂ gasification decreased due to



(a): Needles and branches

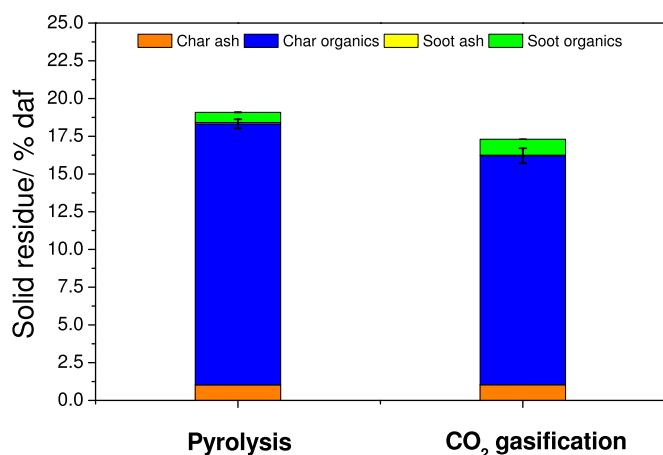
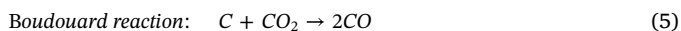
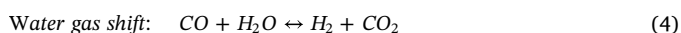
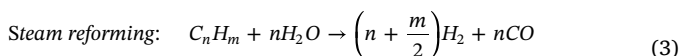
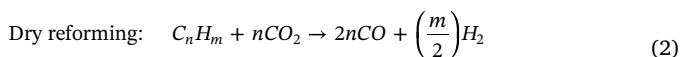
(b): Pyrolysis and gasification of scCO₂ extracted branches

Fig. 3. Soot and char yields (wt% relative to original feedstock) from pyrolysis of: (a) needles and branches and samples after scCO₂ extraction) and (b) from pyrolysis and CO₂ gasification of scCO₂ branches char that was prior treated in the microwave reactor. The total yield of soot and char is separated in ash and organic matters. The error bars characterize the deviations between the total yields of the char and soot.

the heterogeneous Boudouard reaction (Eq. (5)), whereas the reaction between solid carbon and CO₂ increased the formation of CO. Likewise, the H₂ concentration decreased due to the water-gas-shift reaction (Eq. (4)) at temperatures above 1100°C and at residence time less than 3 s, confirming the previous results [65,66].



3.3. Extractives yields

Total amounts of extractives are shown in Fig. 4. The largest amount of extractives (11 wt%, db) was determined in needles, whereas the

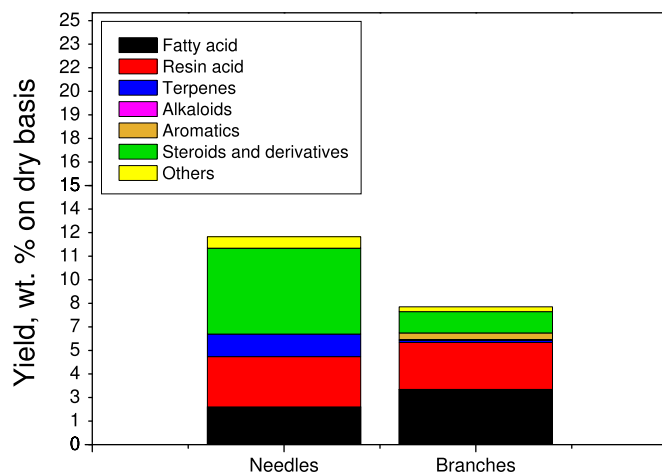


Fig. 4. Yields of non-treated wood fraction extractives. The yields were determined using a Soxhlet apparatus.

extractives content was significantly lower in branches (about 7 wt%, db), corresponding to results of Matisons et al. [67,68].

The extraction of needles led to significantly greater yields of steroids and terpenes than the extraction of branches. The major compositional difference of pinewood needles to other wood fractions is the high content of terpenes, which are represented by monoterpenes, numerous sesquiterpenes, diterpenoids and their derivatives, as reported previously [69]. The extraction of branches showed a greater yield of fatty acids which were mainly represented by hexadecanoic acids. The pinewood branches can include knots with the high content of resin acids and lignans. However, the content of lignans in branches is essentially lower than in knots [55]. The resin derivatives in branches extractives are mainly represented by the abietane group, as previously detected by Backlund et al. [31].

3.4. Py-GC/MS analysis

The formation of main compounds in needles and branches pyrolysis was investigated by Py-GC/MS. The relative peak areas of 27 identified compounds were categorized as acid, ketone, aldehyde, furan, phenol and other products as shown in Fig. 5. The results

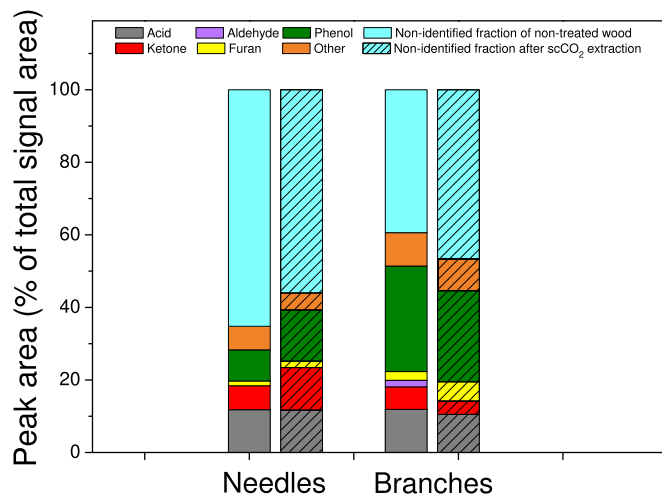


Fig. 5. Relative peak area of volatile products at 600°C using Py-GC/MS shown in % of total chromatographic peak area. The identified peaks are grouped in acid, ketone, aldehyde, furan, phenol, other and non-identified product fractions. The results are shown for non-treated wood fraction (plain) and samples after scCO₂ extraction (striped pattern).

indicated that the relative compositions of volatiles were nearly similar for all wood fractions. The compounds in pyrolysis vapor are all oxygenated chemicals, due to the large amount of oxygen in biomass. The other identified pyrolysis products are methyl glyoxal, levoglucosan, acetamide, N - methyl - N - [4 - (3 - hydroxypyrrolidinyl) - 2 - butynyl], phorbol, and retinoyl glucuronide. The compounds from functional groups of acids, ketones, and phenols were the dominating products in both non-treated wood fractions and samples after scCO₂ extraction. The high concentration of acetic acid was generated from elimination of the acetyl groups originally linked to the xylose unit [70]. Ketone and aldehyde compounds are the main products of secondary volatiles, whose small molecular products were derived from monosaccharides breakdown. The cellulose forms levoglucosan in the first step by the depolymerization, then undergoes dehydration and isomerization reaction to form anhydrosugars [71].

The anhydrosugars further react to form acids, furans, and aldehydes by dehydration, fragmentation and condensation reactions, respectively [72]. The breakdown of glycosidic bonds and the rearrangement of cellulose monomer resulted in the formation of levoglucosan only in potassium lean branches ($K^+ \approx 0.33$ wt%). Interestingly, levoglucosan was not detected in potassium rich needles ($K^+ \approx 1.1$ wt%) during Py/GC-MS analysis [73]. This indicates that potassium plays a minor role on the levoglucosan formation.

3.5. TG-FTIR analysis

The volatiles emitted during the pyrolysis of non-treated needles and branches and samples after scCO₂ extraction were characterized by FTIR spectroscopy. The gas concentrations were not quantified.

However, since the FTIR measurements were conducted under similar pyrolysis conditions, the gas release profiles for the different wood fractions were compared. The FTIR spectra of both fractions were recorded at 300°C, corresponding to the average temperature of the primary devolatilization reactions [74], which are shown in Fig. 6. The condensable gases contain water (4000–3500 cm⁻¹, 1900–1300 cm⁻¹) and primary tars [75]. The water includes both free and bound water. The broad absorption bands (3050–2850 cm⁻¹, 1450–1200 cm⁻¹, 1100–960 cm⁻¹) are characteristic for the absorption of alcohols [51]. The hydroxyl (-OH) region (1300–1000 cm⁻¹) represents the absorption of carboxylic acids, esters, ethers, and alcohols [76]. Light tars containing carboxyl groups such as acetic and formic acid can be formed from the degradation of holocelluloses, and methanol is formed from the methoxy groups (-OCH₃) of lignin [77]. The relative compositions of volatiles were nearly similar for needles and branches forming aldehydes, ketones, acids, and esters between 1900 and 1600 cm⁻¹ and acids and aromatics between 1400 and 1200 cm⁻¹. Methane can be

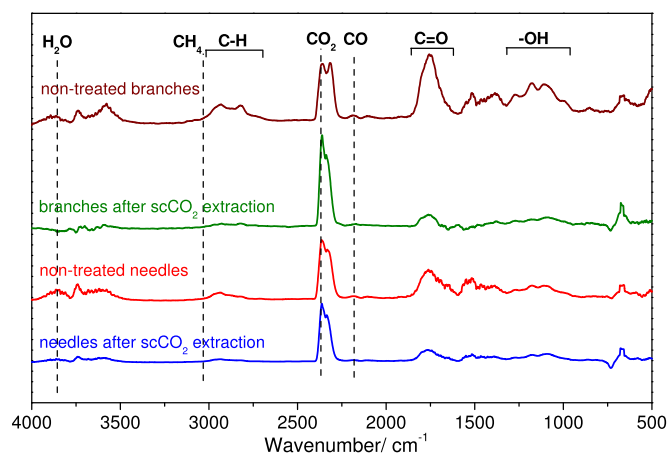
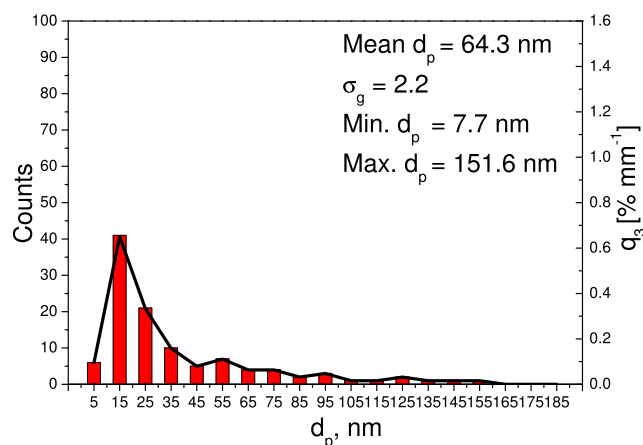
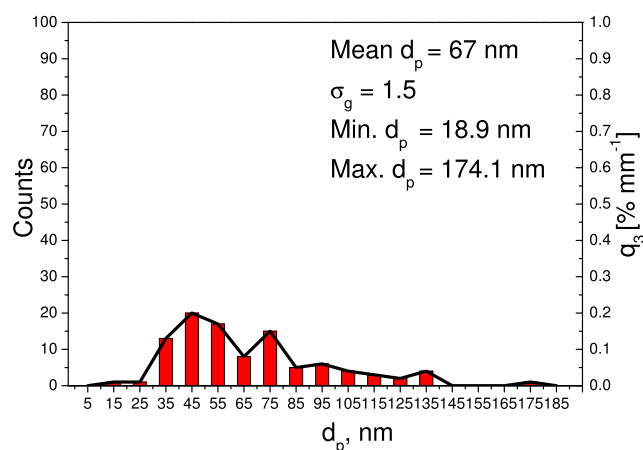


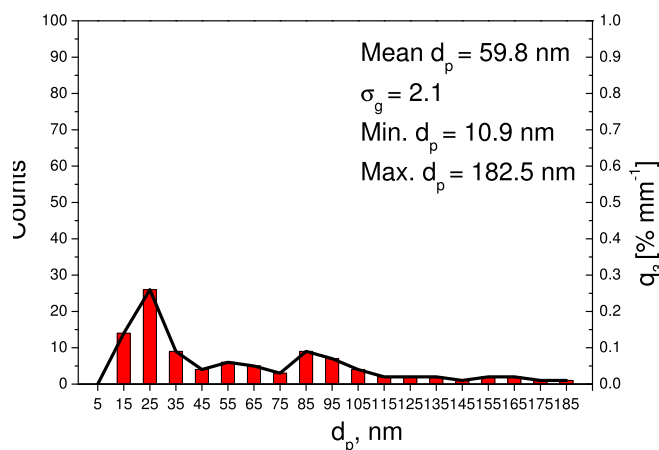
Fig. 6. TG-FTIR of non-treated pinewood fractions and samples after scCO₂ extraction.



(a): Soot from needles after scCO₂



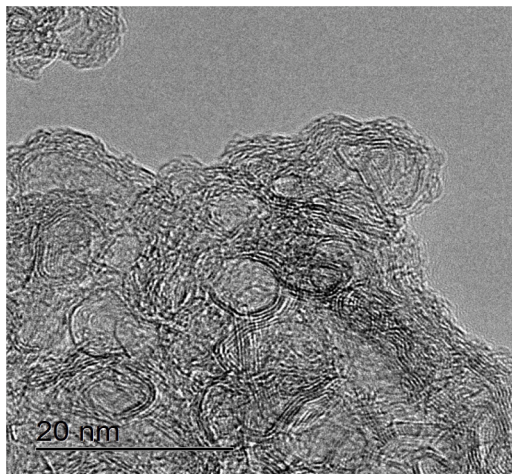
(b): Soot from non-treated branches



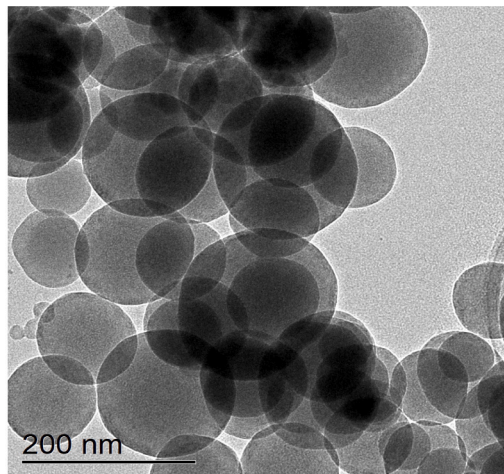
(c): Soot from branches after scCO₂

Fig. 7. Particle size distributions of soot from needles and branches after scCO₂ extraction and non-treated branches.

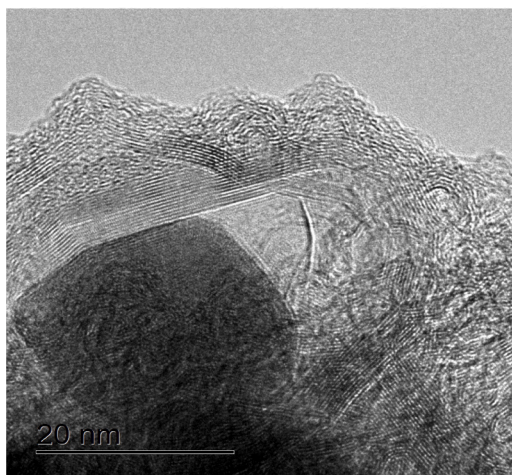
formed at temperatures above 600°C [78] by the cracking of weakly bonded methoxy groups [79]. The TG-FTIR band of non-treated wood fractions showed an absorption band of methane between 3150 and 2850 cm⁻¹, whereas this band is not present during TG-FTIR analysis of wood fractions from scCO₂ extraction. The results indicate that the weak methoxy groups were removed by the supercritical scCO₂ pretreatment at temperatures below 530°C, as shown in the supplemental



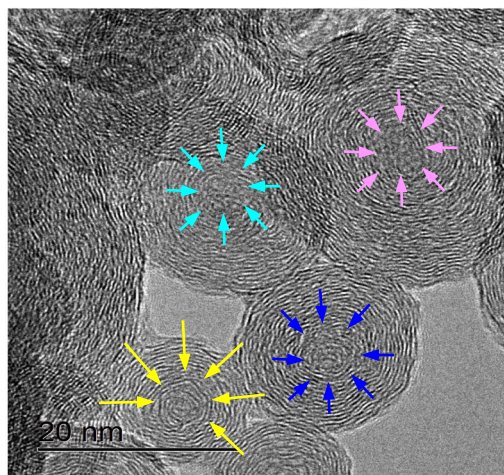
(a): Non-treated needles soot



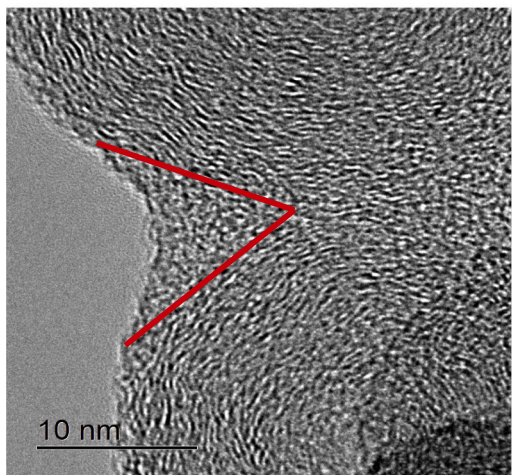
(b): ScCO₂ extracted branches soot



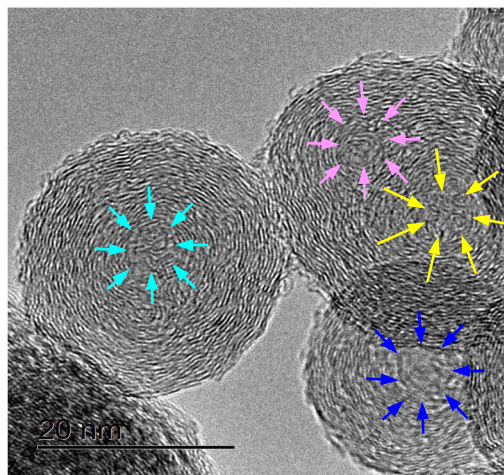
(c): Non-treated needles soot



(d): ScCO₂ extracted needles



(e): Non-treated branches soot



(f): ScCO₂ extracted branches soot

Fig. 8. TEM images of soot generated from non-treated needles and branches and samples after scCO₂ extraction. In (d) and (f) the arrows indicate the soot particle cores. In (e) the red lines indicate a separation of two different carbon structures. (For interpretation of the references to colour in this figure legend, the reader is referred to the web version of this article.)

material (Figs. S-4 and S-5).

3.6. Particle size analysis

Fig. 7 contains plots of the size distributions of primary soot particles plotted as fractions of the number of particles in each size range.

The calculated geometric mean diameters varied from 59.8 to 67 nm, and were similar to the values reported for the soot obtained from pyrolysis of wood and wheat straw (30.8–77.7 nm) [43]. The particle size of non-treated soot needles was not possible to determine due to their non-spherical shape. The soot particles after scCO₂ extraction of needles and branches appeared to be densely fused together with more irregular edges indicating a similar nanostructure to soot particles from hemicellulose pyrolysis [80].

3.7. Soot nanostructure

The nanostructure of the soot from non-treated needles and branches and scCO₂ extracted fractions was studied by TEM. Fig. 8(a), (b) show representative images. In all cases, the soot particles appear as agglomerates, ranging from well-defined primary particles as in scCO₂ extracted soot branches to agglomerates with almost non-visible primary particles as in non-treated needles. Primary soot particles exhibited a core-shell structure, with mostly single cores and a low fraction of multiple cores, as shown in Fig. 8(f).

TEM analysis indicates that both the fine and large primary soot particles consisted of graphene sheets, which grow circumferentially from the particle core. At the contact surfaces of these primary particles an almost amorphous structure appears, gluing together these particles, as shown in Fig. 8(e). Fig. 8(d), (f) show that the particle cores consist mainly of randomly oriented and curved graphene layers. Non-treated soot needles do not show the same circumferential structure with a wavy graphitic structure spanning over the whole agglomerate. All soot samples contained two different carbon structures.

The graphene segments of soot from non-treated branches and scCO₂ extracted needles and branches were well-ordered and flat with the smaller curvature of an average particle size (0.9–0.98; flat graphene ≈ 1 [81]). Table 4 summarizes the characteristics of different soot samples with regards to single or/and multiple cores, curvature and separation distance of graphene layers. The mean separation distance of soot graphene segments (0.35 nm) was slightly greater than that of graphite (0.335 nm) [82]. The mean separation distance of non-treated soot needles was similar to that of pinewood soot and graphite (0.33 nm) [43]. The non-treated soot needles consisted of the longest graphene segments (13.2 nm) with the lower curvature compared to other soot samples, indicating the arrangement of soot nanostructure in both onion rings and straight ribbon structures.

The results demonstrate that the extractives composition is the main factor influencing the nanostructure of soot. The alkali metal content had less influence on the soot nanostructure due to the small difference

in the inorganic composition of raw needles and branches and fractions after scCO₂ extraction. Previous studies showed that low separation distances (close to that of graphite) and high periodicity lead to lower oxidation of carbon materials, while the more bent graphene layers might enhance the reactivity [82,83]. Compared to soot from non-treated branches, the non-treated soot from needles pyrolysis showed a more curved structure with the longer graphene layers, indicating either a higher porosity or larger fraction of amorphous carbon [84,85]. Moreover, soot particles from scCO₂ extracted needles contained more single core structures than soot from non-treated needles with the less recognizable core. The straight graphene layers of the neighboring soot particles from non-treated needles appear to be merged, forming a continuous surface with a large number of crystallites. The extractives removal from needles led to the formation of a soot nanostructure that is similar to scCO₂ extracted soot branches. The greater yields of steroids and terpenes during the scCO₂ extraction of needles than during the extraction of branches and the similar nanostructure of soot from extracted needles and branches strongly suggest the influence of extractives on the soot nanostructure. In addition, analysis of extract composition shows that the resin acids and steroids compounds are the most probable cause for the agglomeration due to the presence of double bonds and carbonyl groups. FTIR analysis showed that double bond and carbonyl functional groups were removed during scCO₂ extraction and thus, soot particles from scCO₂ extracted wood fractions were less agglomerated than those from non-treated wood. The removal of extractives from wood fractions reduced soot agglomeration and decreased particle size of soot, leading to formation of a structure that is similar to fullerene. However, the separation distance of the graphene layers of soot from non-treated samples and scCO₂ extracted wood remained similar to graphite (0.335 nm).

3.8. Char and soot reactivity

Fig. 9 shows differential weight loss curves (DTG) for the 40% volume fraction CO₂ gasification of solid residues from pyrolysis of non-treated needle and branch, samples after scCO₂ extraction, and microwave char reacted in the drop tube furnace. The DTG curves show a single broad peak in CO₂ gasification, indicating a heterogeneous soot mixture with respect to the composition and particle size as suggested by Russell et al. [86]. The maximal reaction rates of both branches and needles solid fractions varied from 850 to 900°C, whereas the maximum reaction rate of non-treated microwave char was about 140°C less than that of microwave char reacted in the DTF, indicating an increase in the char graphitization with the additional heat treatment.

Overall, the thermogravimetric analysis showed that solid residues collected from pyrolysis of wood fractions after scCO₂ were similarly reactive in CO₂ gasification to solid residues generated from non-treated samples. This indicates less significant effect of scCO₂ pretreatment on the CO₂ reactivity of solid residues. The maximal reaction rate of both soot and char samples from heat treatment of non-treated

Table 4

Summary of soot characteristics using TEM (core, curvature, separation distance) prepared from non-treated needles and branches and samples after scCO₂ extraction.

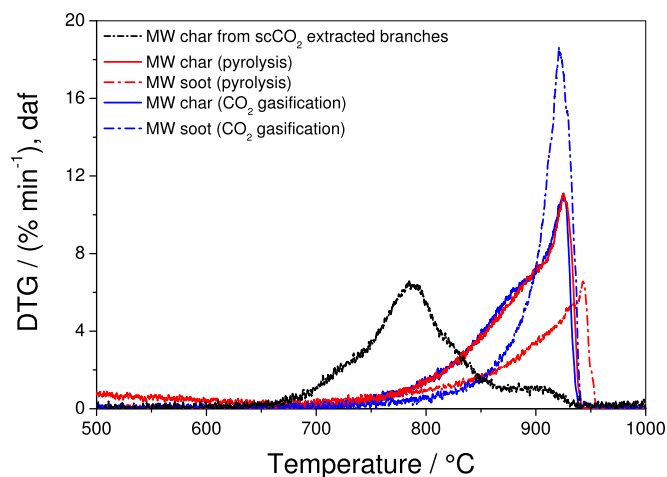
Soot	Fiber length	Curvature ^b	d _{sep} ^{a,b}	Core ^{c,d}
	nm		nm	
Non-treated needles	13.2 ± 7.9	0.7 ± 0.33	0.33 ± 0.01	No clear core
ScCO ₂ extracted needles	4.1 ± 2.3	0.9 ± 0.01	0.35 ± 0.01	s
Non-treated branches	5.1 ± 2.9	0.87 ± 0.04	0.35 ± 0.01	m & mostly s
ScCO ₂ extracted branches	5.2 ± 3.5	0.84 ± 0.05	0.35 ± 0.01	m & mostly s

^a Separation distance.

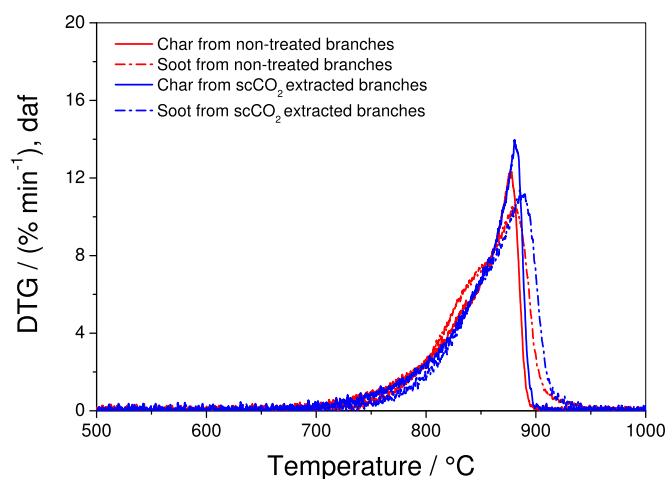
^b Calculation of mean curvature and d_{sep} of graphene layers measured only on crystallites.

^c s - single core and

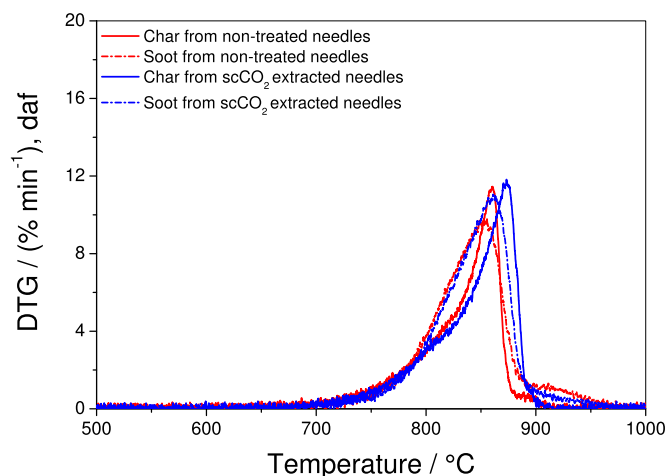
^d m - multiple cores.



9(a): Microwave reacted char from branches



9(b): Branches



9(c): Needles

Fig. 9. (a)–(c) DTG curves of char and soot from pyrolysis and CO₂ gasification of microwave reacted char and from pyrolysis of non-treated needles and branches and samples after scCO₂ extraction reacted in 40% volume fraction CO₂ + 60% volume fraction N₂.

and scCO₂ extracted wood fraction of the same origin remained also similar except the solid residues from the microwave pretreatment.

The r_{max} values for the char from pyrolysis or CO₂ gasification of microwave pre-treated branches varied from 1.3 to 1.5 s⁻¹, whereas the r_{max} values for the soot samples generated under similar conditions ranged from 0.6 to 0.7 s⁻¹, corresponding to the previous results [43]. The CO₂ reactivity of both char and soot from microwave pretreated branches and further reacted under pyrolysis and CO₂ gasification in the DTF was almost similar, as shown in the supplemental material (Table S-2). This indicates less influence of the heat treatment atmosphere on the CO₂ reactivity of microwave pretreated feedstocks. The maximal reaction rate of char and soot from needles was almost 80 times greater than that of solid residues from pyrolysis of branches in the drop tube reactor, as shown in the supplemental material (Table S-2). This emphasizes the importance of the feedstock origin on the CO₂ reactivity of soot and char. This study showed that the differences in nanostructure of soot had no influence on the soot reactivity and might be related to the similar separation distance of graphene layers. However, the composition of original feedstock and microwave pretreatment had a stronger influence on the CO₂ reactivity of collected solid residues than the differences in nanostructure, scCO₂ extraction and heat treatment atmosphere.

3.9. Process overview

The total yield of products after scCO₂ extraction, microwave activation and CO₂ gasification of pinewood branches is shown in Fig. 9. The combination of scCO₂ extraction allows 3.6% of extractives to be obtained from branches that can be potentially used for value-added chemicals. In addition, the low temperature microwave activation of scCO₂ extracted residue provides a novel route to bio-oil production that can be integrated as a part of biorefinery due to the high yield of liquid products (25.2%). Supercritical carbon dioxide has been demonstrated as an effective solvent for the extraction of several products on an industrial scale including hops, coffee and spices [10]. More recently supercritical extraction with carbon dioxide has been demonstrated to be an effective pre-treatment for biomass prior to downstream processing as part of an integrated biorefinery [4,87]. Economic assessments of such processes have been shown to be commercially viable when used in combination with other biorefinery technologies for the production of value added products. Extraction of wood has been shown to reduce potentially hazardous auto-oxidation that can take place during storage [3,88]. As such, if supercritical extraction could be utilized as part of an integrated biorefinery its application on a commercial scale could be viable and would lead to the production of valuable additional products (Fig. 10). In contrast, microwaves have for a long time been employed as an effective heating method on an industrial scale for heating in the food industry.

Pilot continual microwave pyrolysis systems already operate at a multiple kg per hour scales and recent studies have explored the potential to scale microwave pyrolysis to an industrial capacity [89]. Although further research is needed to prove the application of microwave pyrolysis and gasification at scale, this technology does offer significant potential to produce higher value bio-products in a shorter residence time when compared to conventional pyrolysis. The combination of supercritical carbon dioxide extraction coupled with microwave pyrolysis would be attractive technologies for valuable chemicals production as part of a future integrated biorefinery.

4. Conclusion

The novelty of this work relies on the fact that the scCO₂ extraction of wood increases syngas yield in gasification and generates soot particles with the fullerene-like structure. Optimized extraction conditions based on the amount of fatty and resin acids remaining in the pinewood fractions following supercritical treatment enabled the extraction of

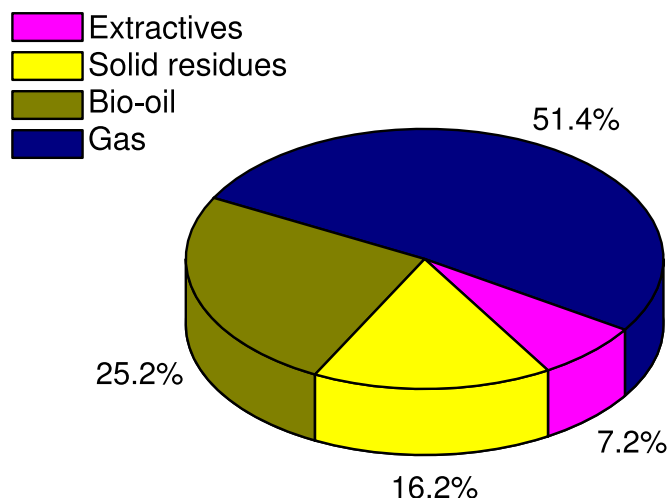


Fig. 10. Total yield of products after scCO₂ extraction, microwave pyrolysis and CO₂ gasification of pinewood branches.

more than half of these compounds. Overall, the low temperature microwave activation of scCO₂ extracted wood samples provided a novel and energy efficient route to bio-oils and feedstock with excellent properties for gasification. The differences in lignocellulosic composition of wood fractions affected the nanostructure of soot more than the alkali metal content that remained only slightly changed after scCO₂ extraction. Therefore, the wood pre-treatment under scCO₂ extraction conditions and microwave pyrolysis have potential to increase a syngas production during entrained flow gasification with the minimal influence on the solid product yields and their reactivity in CO₂ gasification.

CRedit authorship contribution statement

Anna Trubetskaya: Conceptualization, Formal analysis, Investigation, Data curation, Writing - original draft, Writing - review & editing, Visualization, Funding acquisition. **Andrew J. Hunt:** Conceptualization, Investigation, Resources, Writing - review & editing, Supervision, Funding acquisition. **Vitaliy L. Budarin:** Conceptualization, Formal analysis, Funding acquisition. **Thomas M. Attard:** Software, Validation, Formal analysis, Data curation, Writing - review & editing. **Gerrit R. Surup:** Software, Writing - original draft. **Mehrdad Arshadi:** Methodology, Validation, Resources, Project administration, Funding acquisition. **Kentaro Umeki:** Methodology, Resources, Supervision, Funding acquisition.

Declaration of competing interest

None.

Acknowledgements

The authors gratefully acknowledge financial support from FORMAS (CETEX project), Kempe Foundation, Björn Wahlströms, and Jernkontoret Stiftelsen. TEM work was performed at DTU Danchip/Cen the National Center for Micro and Nanofabrication at the Technical University of Denmark. We acknowledge Dr. Daniel Eriksson from Swedish Academy of Agricultural Sciences in Umeå for the preparation of pinewood fractions. Dr. Andrew Hunt would like to acknowledge the financial support of the Thailand Research Fund (RSA6280031) and Khon Kaen University. Financial support from the Center of Excellence for Innovation in Chemistry (PERCH-CIC), Ministry of Higher Education, Science, Research and Innovation is gratefully acknowledged. All authors have read and agreed to the published version of the manuscript

Appendix A. Supplementary data

Supplementary data to this article can be found online at <https://doi.org/10.1016/j.fuproc.2020.106633>.

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